

# Dynamics of Open Chains

CS 6301 Special Topics: Introduction to Robot Manipulation and Navigation

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# Robot Dynamics

- Study motion of robots with the forces and torques that cause them
  - Newton's second law  $F = ma$
- Forward dynamics
  - Given robot state  $(\theta, \dot{\theta})$  and the joint forces and torques  $\mathcal{T}$  Simulation
  - Determine the robot's acceleration  $\ddot{\theta}$
- Inverse dynamics
  - Given robot state  $(\theta, \dot{\theta})$  and a desired acceleration  $\ddot{\theta}$  (from motion planning)
  - Find the joint forces and torques  $\mathcal{T}$  Control

# Dynamics of a Single Rigid Body

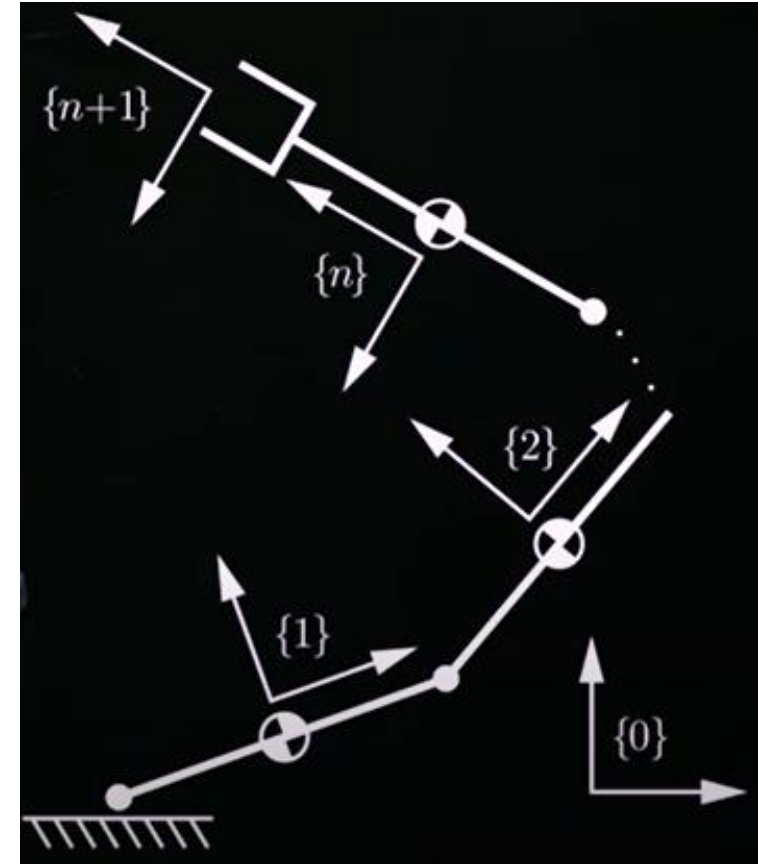
- Inverse dynamics  $\mathcal{F}_b = \mathcal{G}_b \dot{\mathcal{V}}_b - [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b \mathcal{V}_b$
- Forward dynamics  $\dot{\mathcal{V}}_b = \mathcal{G}_b^{-1} (\mathcal{F}_b + [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b \mathcal{V}_b)$

Body wrench  $\mathcal{F}_b = \begin{bmatrix} m_b \\ f_b \end{bmatrix}$       Body twist  $\mathcal{V}_b = \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$

Spatial inertia matrix  $\mathcal{G}_b = \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & mI \end{bmatrix}$        $[\text{ad}_{\mathcal{V}}] = \begin{bmatrix} [\omega] & 0 \\ [v] & [\omega] \end{bmatrix} \in \mathbb{R}^{6 \times 6}$

# Inverse Dynamics of Open Chains

- N-link open chain
- A body-fixed reference frame  $\{i\}$  is attached to the center of mass of each link  $i$
- Base frame  $\{0\}$ , end-effector frame  $\{n+1\}$  (fixed in  $\{n\}$ )

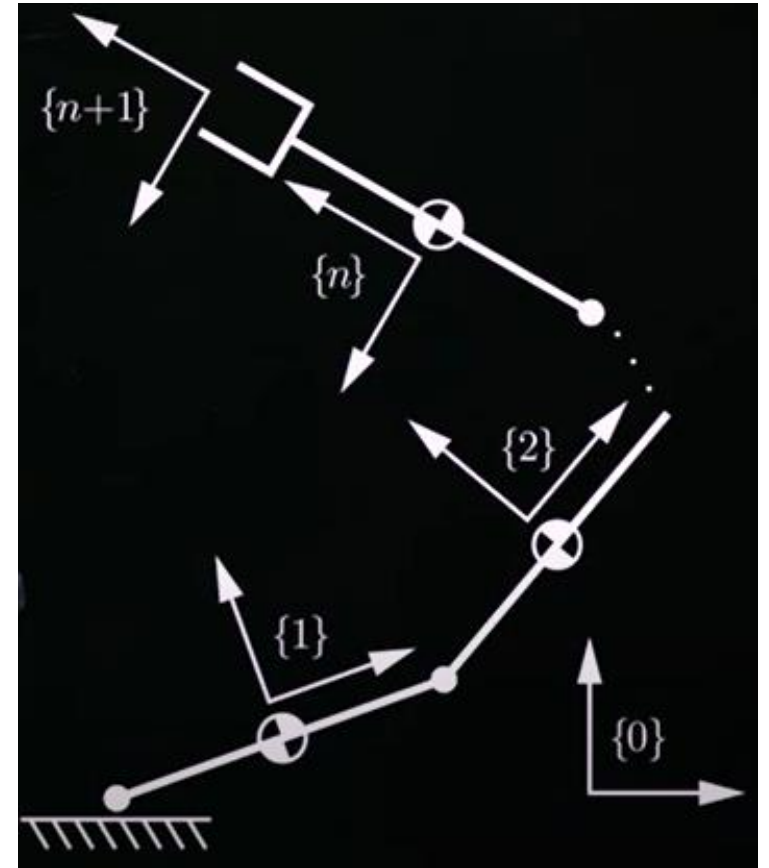


# Inverse Dynamics of Open Chains

- At home position (all joints are zeros)
  - Configuration of frame  $\{j\}$  in  $\{i\}$   $M_{i,j} \in SE(3)$
  - Configuration of  $\{i\}$  in base frame  $\{0\}$   $M_i = M_{0,i}$

$$M_{i-1,i} = M_{i-1}^{-1} M_i$$

$$M_{i,i-1} = M_i^{-1} M_{i-1}$$

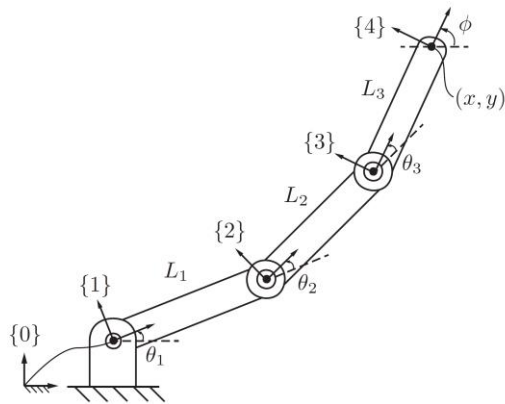


# Inverse Dynamics of Open Chains

- Screw axis for joint  $i$  in link frame  $\{i\}$   $\mathcal{A}_i$ , in space frame  $\{0\}$   $\mathcal{S}_i$

$$\mathcal{A}_i = \text{Ad}_{M_i^{-1}}(\mathcal{S}_i)$$

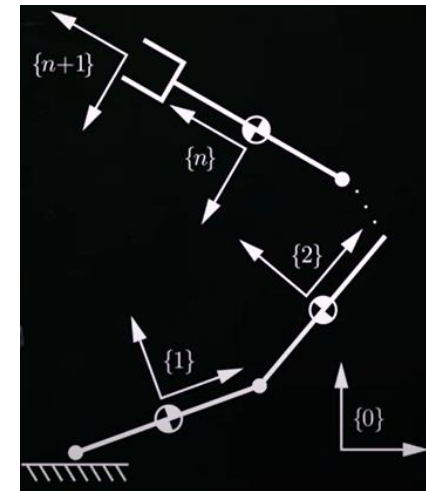
- Recall screw axis



$$\mathcal{S}_a = [\text{Ad}_{T_{ab}}] \mathcal{S}_b$$

$$\mathcal{S}_3 = \begin{bmatrix} \omega_3 \\ v_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ -(L_1 + L_2) \\ 0 \end{bmatrix}$$

$$[\text{Ad}_T] = \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$



# Inverse Dynamics of Open Chains

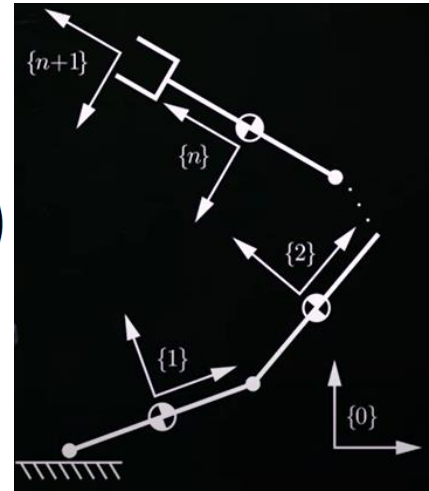
- Screw axis for joint  $i$  in link frame  $\{i\}$   $\mathcal{A}_i$ , in space frame  $\{0\}$   $\mathcal{S}_i$
- The configuration of  $\{j\}$  in  $\{i\}$  with joint variables  $T_{i,j} \in SE(3)$

$$T_{i-1,i}(\theta_i) \quad T_{i,i-1}(\theta_i) = T_{i-1,i}^{-1}(\theta_i)$$

$$T_{i-1,i}(\theta_i) = M_{i-1,i} e^{[\mathcal{A}_i]\theta_i} \quad T_{i,i-1}(\theta_i) = e^{-[\mathcal{A}_i]\theta_i} M_{i,i-1}$$

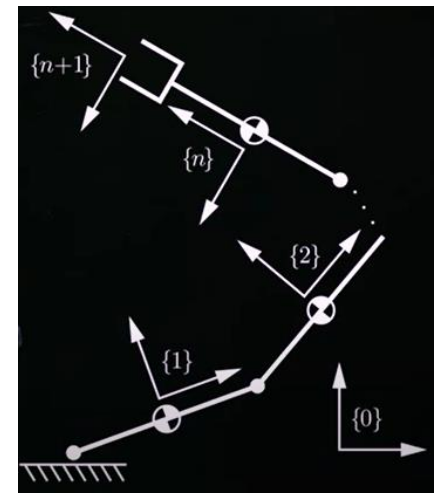
- Twist of link frame  $\{i\}$  expressed in  $\{i\}$   $\mathcal{V}_i = (\omega_i, v_i)$
- Wrench transmitted through joint  $i$  to link frame  $\{i\}$  expressed in  $\{i\}$

$$\mathcal{F}_i = (m_i, f_i)$$



# Inverse Dynamics of Open Chains

- Spatial inertia matrix of link  $i$   $\mathcal{G}_i \in \mathbb{R}^{6 \times 6}$   $\mathcal{G}_i = \begin{bmatrix} \mathcal{I}_i & 0 \\ 0 & m_i I \end{bmatrix}$
- Recursively calculate the twist and acceleration, moving from the base to the tip



$$\mathcal{V}_i = \mathcal{A}_i \dot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \mathcal{V}_{i-1} \quad (\text{Velocity for link } i)$$

$$\dot{\mathcal{V}}_i = \mathcal{A}_i \ddot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \dot{\mathcal{V}}_{i-1} + \frac{d}{dt} ([\text{Ad}_{T_{i,i-1}}]) \mathcal{V}_{i-1}$$

See Lynch & Park for derivation

$$\dot{\mathcal{V}}_i = \mathcal{A}_i \ddot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \dot{\mathcal{V}}_{i-1} + [\text{ad}_{\mathcal{V}_i}] \mathcal{A}_i \dot{\theta}_i$$

$$[\text{ad}_{\mathcal{V}}] = \begin{bmatrix} [\omega] & 0 \\ [v] & [\omega] \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$



# Inverse Dynamics of Open Chains

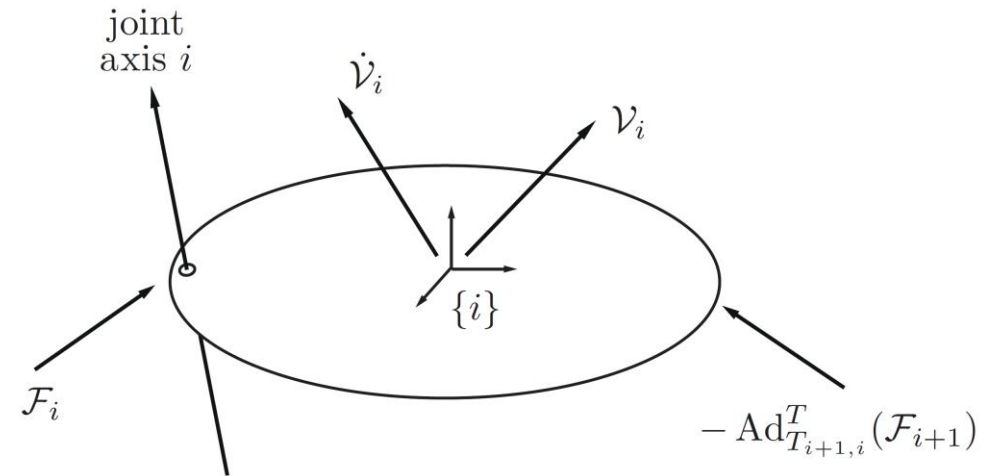
- Accelerations from base to tip

$$\mathcal{F}_b = [\text{Ad}_{T_{ab}}]^T \mathcal{F}_a$$

$$\dot{\mathcal{V}}_i = \mathcal{A}_i \ddot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \dot{\mathcal{V}}_{i-1} + [\text{ad}_{\mathcal{V}_i}] \mathcal{A}_i \dot{\theta}_i$$

- Recall rigid body dynamic equations

$$\begin{aligned} \mathcal{F}_b &= \mathcal{G}_b \dot{\mathcal{V}}_b - \text{ad}_{\mathcal{V}_b}^T (\mathcal{P}_b) \\ &= \mathcal{G}_b \dot{\mathcal{V}}_b - [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b \mathcal{V}_b \end{aligned}$$



- Wrench on link i from joint i and joint i+1

$$\mathcal{G}_i \dot{\mathcal{V}}_i - \text{ad}_{\mathcal{V}_i}^T (\mathcal{G}_i \mathcal{V}_i) = \mathcal{F}_i - \text{Ad}_{T_{i+1,i}}^T (\mathcal{F}_{i+1})$$

# Inverse Dynamics

- Solve the wrench from tip to base  $\mathcal{F}_i$
- Force or torque at the joint in the direction of the joint's screw axis

$$\tau_i \dot{\theta}_i = \mathcal{F}_i^T \mathcal{A}_i \dot{\theta}_i$$

Principle of conservation of power

$$\tau_i = \mathcal{F}_i^T \mathcal{A}_i$$

- Newton-Euler Inverse Dynamics Algorithm

# Newton-Euler Inverse Dynamics Algorithm

Given  $\theta, \dot{\theta}, \ddot{\theta}$  Compute  $\mathcal{T}$

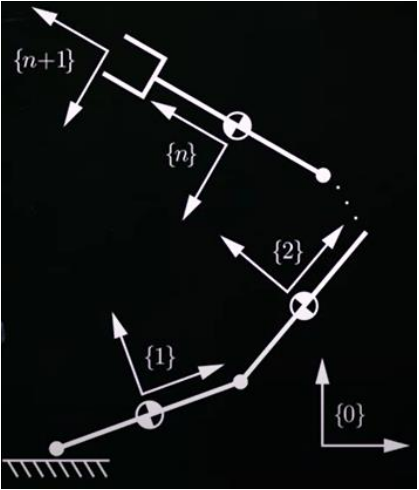
**Forward iterations** Given  $\theta, \dot{\theta}, \ddot{\theta}$ , for  $i = 1$  to  $n$  do

$$\begin{aligned} \mathcal{V}_0 &= (0, 0) & T_{i,i-1} &= e^{-[\mathcal{A}_i]\theta_i} M_{i,i-1}, \\ \dot{\mathcal{V}}_0 &= (0, -g) & \mathcal{V}_i &= \text{Ad}_{T_{i,i-1}}(\mathcal{V}_{i-1}) + \mathcal{A}_i \dot{\theta}_i, \\ & & \dot{\mathcal{V}}_i &= \text{Ad}_{T_{i,i-1}}(\dot{\mathcal{V}}_{i-1}) + \text{ad}_{\mathcal{V}_i}(\mathcal{A}_i) \dot{\theta}_i + \mathcal{A}_i \ddot{\theta}_i. \end{aligned}$$

**Backward iterations** For  $i = n$  to 1 do

$$\begin{aligned} \mathcal{F}_{n+1} &= \mathcal{F}_{\text{tip}} \\ &= (m_{\text{tip}}, f_{\text{tip}}) & \mathcal{F}_i &= \text{Ad}_{T_{i+1,i}}^T(\mathcal{F}_{i+1}) + \mathcal{G}_i \dot{\mathcal{V}}_i - \text{ad}_{\mathcal{V}_i}^T(\mathcal{G}_i \mathcal{V}_i), \\ & & \tau_i &= \mathcal{F}_i^T \mathcal{A}_i. \end{aligned}$$

The wrench applied to the environment by the end-effector



# Dynamics Equations in Closed Form

- Dynamic equations  $\tau = M(\theta)\ddot{\theta} + C(\theta, \dot{\theta})\dot{\theta} + g(\theta)$
- Definitions

$$\mathcal{V} = \begin{bmatrix} \mathcal{V}_1 \\ \vdots \\ \mathcal{V}_n \end{bmatrix} \in \mathbb{R}^{6n} \quad \mathcal{F} = \begin{bmatrix} \mathcal{F}_1 \\ \vdots \\ \mathcal{F}_n \end{bmatrix} \in \mathbb{R}^{6n} \quad \mathcal{A} = \begin{bmatrix} \mathcal{A}_1 & 0 & \cdots & 0 \\ 0 & \mathcal{A}_2 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & \cdots & \cdots & \mathcal{A}_n \end{bmatrix} \in \mathbb{R}^{6n \times n}$$

$$\mathcal{G} = \begin{bmatrix} \mathcal{G}_1 & 0 & \cdots & 0 \\ 0 & \mathcal{G}_2 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & \cdots & \cdots & \mathcal{G}_n \end{bmatrix} \in \mathbb{R}^{6n \times 6n} \quad [\text{ad}_{\mathcal{V}}] = \begin{bmatrix} [\text{ad}_{\mathcal{V}_1}] & 0 & \cdots & 0 \\ 0 & [\text{ad}_{\mathcal{V}_2}] & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & \cdots & \cdots & [\text{ad}_{\mathcal{V}_n}] \end{bmatrix} \in \mathbb{R}^{6n \times 6n}$$

$$[\text{ad}_{\mathcal{A}\dot{\theta}}] = \begin{bmatrix} [\text{ad}_{\mathcal{A}_1\dot{\theta}_1}] & 0 & \cdots & 0 \\ 0 & [\text{ad}_{\mathcal{A}_2\dot{\theta}_2}] & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & \cdots & \cdots & [\text{ad}_{\mathcal{A}_n\dot{\theta}_n}] \end{bmatrix} \in \mathbb{R}^{6n \times 6n} \quad \mathcal{W}(\theta) = \begin{bmatrix} 0 & 0 & \cdots & 0 & 0 \\ [\text{Ad}_{T_{21}}] & 0 & \cdots & 0 & 0 \\ 0 & [\text{Ad}_{T_{32}}] & \cdots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & [\text{Ad}_{T_{n,n-1}}] & 0 \end{bmatrix} \in \mathbb{R}^{6n \times 6n}$$

# Dynamics Equations in Closed Form

$$\mathcal{V}_{\text{base}} = \begin{bmatrix} \text{Ad}_{T_{10}}(\mathcal{V}_0) \\ 0 \\ \vdots \\ 0 \end{bmatrix} \in \mathbb{R}^{6n} \quad \dot{\mathcal{V}}_{\text{base}} = \begin{bmatrix} \text{Ad}_{T_{10}}(\dot{\mathcal{V}}_0) \\ 0 \\ \vdots \\ 0 \end{bmatrix} \in \mathbb{R}^{6n} \quad \mathcal{F}_{\text{tip}} = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ \text{Ad}_{T_{n+1,n}}^T(\mathcal{F}_{n+1}) \end{bmatrix} \in \mathbb{R}^{6n}$$

Recursive inverse dynamics algorithm

$$\begin{aligned} \mathcal{V} &= \mathcal{W}(\theta)\mathcal{V} + \mathcal{A}\dot{\theta} + \mathcal{V}_{\text{base}}, \\ \dot{\mathcal{V}} &= \mathcal{W}(\theta)\dot{\mathcal{V}} + \mathcal{A}\ddot{\theta} - [\text{ad}_{\mathcal{A}\dot{\theta}}](\mathcal{W}(\theta)\mathcal{V} + \mathcal{V}_{\text{base}}) + \dot{\mathcal{V}}_{\text{base}}, \\ \mathcal{F} &= \mathcal{W}^T(\theta)\mathcal{F} + \mathcal{G}\dot{\mathcal{V}} - [\text{ad}_{\mathcal{V}}]^T\mathcal{G}\mathcal{V} + \mathcal{F}_{\text{tip}}, \\ \tau &= \mathcal{A}^T\mathcal{F}. \end{aligned}$$

# Dynamics Equations in Closed Form

• Define  $\mathcal{L}(\theta) = (I - \mathcal{W}(\theta))^{-1}$

$$\mathcal{V} = \mathcal{L}(\theta) \left( \mathcal{A}\dot{\theta} + \mathcal{V}_{\text{base}} \right),$$

$$\dot{\mathcal{V}} = \mathcal{L}(\theta) \left( \mathcal{A}\ddot{\theta} + [\text{ad}_{\mathcal{A}\dot{\theta}}]\mathcal{W}(\theta)\mathcal{V} + [\text{ad}_{\mathcal{A}\dot{\theta}}]\mathcal{V}_{\text{base}} + \dot{\mathcal{V}}_{\text{base}} \right)$$

$$\mathcal{F} = \mathcal{L}^T(\theta) \left( \mathcal{G}\dot{\mathcal{V}} - [\text{ad}_{\mathcal{V}}]^T\mathcal{G}\mathcal{V} + \mathcal{F}_{\text{tip}} \right),$$

$$\tau = \mathcal{A}^T \mathcal{F}.$$

# Dynamics Equations in Closed Form

- If the robot applies an external wrench at the end-effector  $\mathcal{F}_{\text{tip}}$

End-effector torque  $\tau = J^T(\theta)\mathcal{F}_{\text{tip}}$

$$\tau = M(\theta)\ddot{\theta} + c(\theta, \dot{\theta}) + g(\theta) + J^T(\theta)\mathcal{F}_{\text{tip}}$$

$$M(\theta) = \mathcal{A}^T \mathcal{L}^T(\theta) \mathcal{G} \mathcal{L}(\theta) \mathcal{A},$$

$$c(\theta, \dot{\theta}) = -\mathcal{A}^T \mathcal{L}^T(\theta) (\mathcal{G} \mathcal{L}(\theta) [\text{ad}_{\mathcal{A}\dot{\theta}}] \mathcal{W}(\theta) + [\text{ad}_{\mathcal{V}}]^T \mathcal{G}) \mathcal{L}(\theta) \mathcal{A} \dot{\theta},$$

$$g(\theta) = \mathcal{A}^T \mathcal{L}^T(\theta) \mathcal{G} \mathcal{L}(\theta) \dot{\mathcal{V}}_{\text{base}}.$$

# Robot Dynamics

- Study motion of robots with the forces and torques that cause them
- Equations of motion
  - A set of second-order differential equations

$$\tau = M(\theta)\ddot{\theta} + h(\theta, \dot{\theta}) \quad \text{Joint variables } \theta \in \mathbb{R}^n$$

Joint forces and torques  $\tau \in \mathbb{R}^n$        $M(\theta) \in \mathbb{R}^{n \times n}$       a symmetric positive-definite **mass matrix**

$h(\theta, \dot{\theta}) \in \mathbb{R}^n$       forces that lump together centripetal, Coriolis, gravity, and friction terms that depend on  $\theta$  and  $\dot{\theta}$



# Forward Dynamics of Open Chains

- Forward dynamics  $M(\theta)\ddot{\theta} = \tau(t) - h(\theta, \dot{\theta}) - J^T(\theta)\mathcal{F}_{\text{tip}}$ 
  - Given  $\theta, \dot{\theta}, \tau, \mathcal{F}_{\text{tip}}$  Solve  $\ddot{\theta}$
- $h(\theta, \dot{\theta})$  can be computed by the inverse dynamics algorithm with  $\ddot{\theta} = 0$  and  $\mathcal{F}_{\text{tip}} = 0$
- We can solve

$$M\ddot{\theta} = b, \text{ for } \ddot{\theta}$$

$$b = \tau(t) - h(\theta, \dot{\theta}) - J^T(\theta)\mathcal{F}_{\text{tip}}$$

# Forward Dynamics of Open Chains

- Simulate the motion of a robot

$$\ddot{\theta} = \text{ForwardDynamics}(\theta, \dot{\theta}, \tau, \mathcal{F}_{\text{tip}})$$

First-order differential equations

$$q_1 = \theta, \quad q_2 = \dot{\theta} \quad \begin{array}{l} \dot{q}_1 = q_2, \\ \dot{q}_2 = \text{ForwardDynamics}(q_1, q_2, \tau, \mathcal{F}_{\text{tip}}) \end{array}$$

First-order Euler iteration

$$q_1(t + \delta t) = q_1(t) + q_2(t)\delta t,$$

$$q_2(t + \delta t) = q_2(t) + \text{ForwardDynamics}(q_1, q_2, \tau, \mathcal{F}_{\text{tip}})\delta t$$

Initial values  $q_1(0) = \theta(0)$  and  $q_2(0) = \dot{\theta}(0)$

# Summary

- Newton-Euler Inverse Dynamics Algorithm
- Forward Dynamics of Open Chains

# Further Reading

- Chapter 8 in Kevin M. Lynch and Frank C. Park. Modern Robotics: Mechanics, Planning, and Control. 1st Edition, 2017.
- Dynamics of Dynamics of Open Chains: Newton Euler Approach. Prof. Wei Zhang, Southern University of Science and Technology, Shenzhen, China [https://www.wzhanglab.site/wp-content/uploads/2024/06/LN9\\_DynamicsOfOpenChain.pdf](https://www.wzhanglab.site/wp-content/uploads/2024/06/LN9_DynamicsOfOpenChain.pdf)