Forward Kinematics and Denavit-Hartenberg Parameters

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Robot Kinematics

• The relationship between a robot's joint coordinates and its spatial layout

<https://www.marginallyclever.com/2020/04/gradient-descent-inverse-kinematics-for-6dof-robot-arms/>

- Forward kinematics of a robot: calculation of the position and orientation of its end-effector from its joint coordinates $\boldsymbol{\theta}$
- Recall robot links and joints

Forward kinematics of a 3R planar open chain.

- End-effector frame ${4}$
- Joint angles $(\theta_1, \theta_2, \theta_3)$
- Position and orientation of the end-effector frame

$$
L_1 \cos \theta_1 + L_2 \cos(\theta_1 + \theta_2) + L_3 \cos(\theta_1 + \theta_2 + \theta_3),
$$

\n
$$
L_1 \sin \theta_1 + L_2 \sin(\theta_1 + \theta_2) + L_3 \sin(\theta_1 + \theta_2 + \theta_3),
$$

\n
$$
L_2 \sin(\theta_1 + \theta_2) + L_3 \sin(\theta_1 + \theta_2 + \theta_3),
$$

\n
$$
L_3 \sin(\theta_1 + \theta_2 + \theta_3).
$$

Forward kinematics of a 3R planar open chain.

- General cases
	- Attaching frames to links
	- Using homogeneous transformations

$$
T_{04} = T_{01}T_{12}T_{23}T_{34}
$$

$$
I = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & 0 & 0 \\ \sin \theta_1 & \cos \theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} T_{12} = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & L_1 \\ \sin \theta_2 & \cos \theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}
$$

$$
T_{34} = \begin{bmatrix} \cos \theta_3 & -\sin \theta_3 & 0 & L_2 \\ \sin \theta_3 & \cos \theta_3 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} T_{34} = \begin{bmatrix} 1 & 0 & 0 & L_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}
$$

 $T_{i-1,i}$ Depends only on the joint variable θ_i

- Method 1: uses homogeneous transformations
	- Need to define the coordinates of frames
	- Denavit-Hartenberg Parameters

Northwestern Engineering's legacy in robotics started in the 1950s when Dick Hartenberg, a professor, and Jacques Denavit, a PhD student, developed a way to represent mathematically how mechanisms move <https://robotics.northwestern.edu/history.html>

- Method 2: uses screw-axis representations of transformations
	- No need to define frame references
	- Next lecture

Denavit-Hartenberg Parameters

- Attach reference frames to each link of an open chain
- Derive forward kinematics using the relative displacements between adjacent line frames
- For a chain with n 1DOF joints, 0,…,n
	- The ground link is 0
	- The end-effect frame is attached to link n

$$
T_{0n}(\theta_1,\ldots,\theta_n) = T_{01}(\theta_1)T_{12}(\theta_2)\cdots T_{n-1,n}(\theta_n)
$$

$$
T_{i,i-1} \in SE(3)
$$

Denavit-Hartenberg Parameters

• Assigning link frames

- $\hat{\mathbf{z}}_i$ -axis coincides with joint axis i
- $\hat{\mathbf{z}}_{i-1}$ -axis coincides with joint axis i-1
- Origin of the link frame
	- Find the line segment that orthogonally intersects both the joint axes
	- Origin of frame {i-1} is the intersection of the line and the joint axis i-1
- \hat{x} -axis in the direction of the mutual perpendicular line pointing from (i-1)-axis to i-axis
- \hat{y} -axis given by $\hat{x} \times \hat{y} = \hat{z}$

Denavit-Hartenberg (D-H) Parameters

- Link length: the length of the mutual perpendicular line a_{i-1}
	- Not the actual length of the physical link
- Line twist α_{i-1} the angle from \hat{z}_{i-1} to \hat{z}_i , measured about \hat{x}_{i-1}
- Line offset d_i
	- Distance from the intersection to the origin of the link-i frame
- Joint angle ϕ_i

the angle from \hat{x}_{i-1} to \hat{x}_i , measured about the \hat{z}_i -axis

D-H Parameters

- For an open chain with n 1DOF joints, 4n D-H parameters
- For an open chain with all joints revolute
	- Link lengths a_{i-1}
	- Line twists α_{i-1} **Constants**
	- Line offsets d_i
	- Joint angle parameters are the joint variables ϕ_i

D-H Parameters

- When adjacent revolute joint axes intersect
	- No mutual perpendicular line
	- Link length 0
	- \hat{x}_{i-1} perpendicular to the plane spanned by \hat{z}_{i-1} and \hat{z}_i
- When adjacent revolute joint axes are parallel
	- Many possibilities for a mutually perpendicular line
	- Choose the one that is most physically intuitive and results in many zero parameters as possible
- Ground frame and End-Effector frame
	- Choose the one that is most physically intuitive and results in many zero parameters as possible

D-H Parameters

• Prismatic joints

- \hat{z}_i -axis positive direction of translation
	- d_i link offset is the joint variable
	- ϕ_i joint angle is constant
- \hat{x} -axis in the direction of the mutual perpendicular line pointing from (i-1) axis to i-axis
- \hat{y} -axis given by $\hat{x} \times \hat{y} = \hat{z}$

• Link frame transformation

 $= \text{Rot}(\hat{x}, \alpha_{i-1}) \text{Trans}(\hat{x}, a_{i-1}) \text{Trans}(\hat{z}, d_i) \text{Rot}(\hat{z}, \phi_i)$ $T_{i-1,i}$

- (a) A rotation of frame $\{i-1\}$ about its \hat{x} -axis by an angle α_{i-1} .
- A translation of this new frame along its \hat{x} -axis by a distance a_{i-1} . (b)
- A translation of the new frame formed by (b) along its \hat{z} -axis by a distance (c) $d_i.$
- A rotation of the new frame formed by (c) about its \hat{z} -axis by an angle ϕ_i . (d)

• Link frame transformation

• Link frame transformation
\n
$$
T_{i-1,i} = \text{Rot}(\hat{\mathbf{x}}, \alpha_{i-1}) \text{Trans}(\hat{\mathbf{x}}, a_{i-1}) \text{Trans}(\hat{\mathbf{z}}, d_i) \text{Rot}(\hat{\mathbf{z}}, \phi_i)
$$
\n
$$
= \begin{bmatrix}\n\cos \phi_i & -\sin \phi_i & 0 & a_{i-1} \\
\sin \phi_i \cos \alpha_{i-1} & \cos \phi_i \cos \alpha_{i-1} & -\sin \alpha_{i-1} & -d_i \sin \alpha_{i-1} \\
\sin \phi_i \sin \alpha_{i-1} & \cos \phi_i \sin \alpha_{i-1} & \cos \alpha_{i-1} & d_i \cos \alpha_{i-1} \\
0 & 0 & 0 & 1\n\end{bmatrix}
$$
\n
$$
\text{Rot}(\hat{\mathbf{z}}, \phi_i) = \begin{bmatrix}\n\cos \phi_{i-1} & -\sin \phi_{i-1} & 0 & 0 \\
\sin \phi_{i-1} & \cos \phi_{i-1} & 0 & 0 & 0 \\
0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1\n\end{bmatrix}
$$
\n
$$
\text{Trans}(\hat{\mathbf{z}}, a_{i-1}) = \begin{bmatrix}\n1 & 0 & 0 & a_{i-1} \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1 \\
0 & 0 & 0 & 1\n\end{bmatrix}
$$
\n
$$
\text{Trans}(\hat{\mathbf{x}}, a_{i-1}) = \begin{bmatrix}\n1 & 0 & 0 & a_{i-1} \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1\n\end{bmatrix}
$$
\n
$$
\text{Res}(\hat{\mathbf{x}}, a_{i-1}) = \begin{bmatrix}\n1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1 \\
0 & 0 & 0 & 1\n\end{bmatrix}
$$
\n
$$
\text{Res}(\hat{\mathbf{x}}, a_{i-1}) = \begin{bmatrix}\n1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1 \\
0 & 0 & 0 & 1\n\end{bmatrix}
$$
\n
$$
\text{Res}(\hat{\mathbf{x}}, a_{i-1}) = \begin{bmatrix}\n1 & 0 & 0 & 0 \\
0
$$

Joint i

axis $i-1$

An RRRP spatial open chain in its zero position

A 6R spatial open chain in its zero position

 α_{i-1} the angle from \hat{z}_{i-1} to \hat{z}_i , measured about \hat{x}_{i-1} ϕ_i the angle from \hat{x}_{i-1} to \hat{x}_i , measured about the \hat{z}_i -axis

Summary

- Forward kinematics
- Denavit-Hartenberg Parameters

Further Reading

- Chapter 4 and Appendix C in Kevin M. Lynch and Frank C. Park. Modern Robotics: Mechanics, Planning, and Control. 1st Edition, 2017.
- J. Denavit and R. S. Hartenberg. A kinematic notation for lower-pair mechanisms based on matrices. ASME Journal of Applied Mechanics, 23:215-221, 1955.