Robot Control: Motion Control, Force Control, Impedance Control

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NIV

Motion Control of a Multi-joint Robot

• Dynamics
$$au = M(heta) \ddot{ heta} + h(heta, \dot{ heta})$$

 $n \times n$

- Decentralized control
 - Each joint is controlled independently
 - When dynamics are decoupled (approximately)
- Centralized control
 - Full state information for each of the n joints is available to calculate the controls for each joint

Centralized Multi-joint Control

Computed torque controller

$$\tau = \tilde{M}(\theta) \left(\ddot{\theta}_d + K_p \theta_e + K_i \int \theta_e(t) dt + K_d \dot{\theta}_e \right) + \tilde{h}(\theta, \dot{\theta})$$

$$K_p, K_i, K_d \text{ positive-definite matrices} \quad \text{We choose the gain matrices as} \quad k_p I, \ k_i I, \text{ and } k_d I$$

• PID control and gravity compensation

When the model is not good

$$\tau = K_p \theta_e + K_i \int \theta_e(\mathbf{t}) d\mathbf{t} + K_d \dot{\theta}_e + \tilde{g}(\theta)$$

• Motion as a trajectory of the end-effector in the task space

$$(X(t), \mathcal{V}_b(t))$$
 $X \in SE(3)$ $[\mathcal{V}_b] = X^{-1}\dot{X}$ Twist

- Option 1: convert the trajectory to joint space
 - Forward kinematics $X = T(\theta)$ $\mathcal{V}_b = J_b(\theta)\dot{\theta}$ $\dot{\mathcal{V}} = \dot{J}(\theta)\dot{\theta} + J(\theta)\ddot{\theta}$
 - Inverse kinematics

$$\theta(t) = T^{-1}(X(t)),$$

$$\dot{\theta}(t) = J_b^{\dagger}(\theta(t))\mathcal{V}_b(t),$$

$$\ddot{\theta}(t) = J_b^{\dagger}(\theta(t))\left(\dot{\mathcal{V}}_b(t) - \dot{J}_b(\theta(t))\dot{\theta}(t)\right)$$

may require significant computing power

• Task-space dynamics

$$\mathcal{F} = \Lambda(\theta)\dot{\mathcal{V}} + \eta(\theta, \mathcal{V})$$

$$\Lambda(\theta) = J^{-T}M(\theta)J^{-1},$$

$$\eta(\theta, \mathcal{V}) = J^{-T}h(\theta, J^{-1}\mathcal{V}) - \Lambda(\theta)\dot{J}J^{-1}\mathcal{V}.$$

- Option 2: task-space dynamics $\mathcal{F}_b = \Lambda(\theta)\dot{\mathcal{V}}_b + \eta(\theta,\mathcal{V}_b)$
- Joint forces and torques $au = J_b^{
 m T}(heta) \mathcal{F}_b$
- Computed torque controller

Joint space
$$\tau = \tilde{M}(\theta) \left(\ddot{\theta}_d + K_p \theta_e + K_i \int \theta_e(\mathbf{t}) d\mathbf{t} + K_d \dot{\theta}_e \right) + \tilde{h}(\theta, \dot{\theta})$$

Task space $\tau =$

$$J_b^{\mathrm{T}}(\theta) \left(\tilde{\Lambda}(\theta) \left(\frac{d}{dt} ([\mathrm{Ad}_{X^{-1}X_d}] \mathcal{V}_d) + K_p X_e + K_i \int X_e(t) dt + K_d \mathcal{V}_e \right) + \tilde{\eta}(\theta, \mathcal{V}_b) \right)$$

- When the task is to apply forces and torques to the environment
- The manipulator dynamics with applied wrench

$$M(\theta)\ddot{\theta} + c(\theta,\dot{\theta}) + g(\theta) + b(\dot{\theta}) + J^{\mathrm{T}}(\theta)\mathcal{F}_{\mathrm{tip}} = \tau$$
Centripetal & Coriolis Gravity Friction Wrench applied to the environment

- The Robot moves slowly (or not at all) during a force control task
 - Ignore the acceleration and the velocity terms

$$g(\theta) + J^{\mathrm{T}}(\theta)\mathcal{F}_{\mathrm{tip}} = \tau$$

• Without direct measurements of the force-torque at the robot endeffector, by using joint-angle feedback

The force-control law
$$\tau = \tilde{g}(\theta) + J^{\mathrm{T}}(\theta)\mathcal{F}_d$$

A model of the gravitational torques

Desired wrench

• Use a six-axis force-torque sensor between the arm and the end-effector to measure the end-effector wrench $\mathcal{F}_{\rm tip}$



• A PI force controller with a feedforward term and gravity compensation

$$\tau = \tilde{g}(\theta) + J^{\mathrm{T}}(\theta) \left(\mathcal{F}_d + K_{fp} \mathcal{F}_e + K_{fi} \int \mathcal{F}_e(\mathbf{t}) d\mathbf{t} \right)$$

$$\mathcal{F}_e = \mathcal{F}_d - \mathcal{F}_{\mathrm{tip}}$$

Adding velocity damping

$$\tau = \tilde{g}(\theta) + J^{\mathrm{T}}(\theta) \left(\mathcal{F}_{d} + K_{fp} \mathcal{F}_{e} + K_{fi} \int \mathcal{F}_{e}(\mathbf{t}) d\mathbf{t} - K_{\mathrm{damp}} \mathcal{V} \right)$$

• Robot impedance characterizes the change in endpoint motion as a function of disturbance forces.

Impedance
$$R=rac{F}{V}$$
 Force Velocity

- Ideal motion control
 - High impedance, little change in motion due to force disturbances
- Ideal force control
 - Low impedance, little change in force due to motion disturbances

- Impedance control is an approach to dynamic control relating force and position
- The robot end-effector is asked to render particular mass, spring, and damper properties



https://youtu.be/XwiX2vv14Qs

• The dynamics for a one dof robot rendering an impedance



High impedance: b or k is large

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• Goal: implement the task-space behavior

$$M\ddot{x} + B\dot{x} + Kx = f_{\text{ext}}$$

 $x \in \mathbb{R}^n$ Task-space configuration in a minimum set of coordinates

 $M,B, \mathrm{and}\ K$ Positive-definite virtual mass, damping, and stiffness matrices

 f_{ext} Force applied to the robot

Two ways of Impedance Control

$$M\ddot{x} + B\dot{x} + Kx = f_{\text{ext}}$$

- Impedance controlled
 - The robot senses the endpoint motion $\,x(t)\,$
 - Commands joint torques and forces to create $-f_{
 m ext}$
 - Displays the force to the user
- Admittance controlled
 - The robot senses $\,f_{
 m ext}$
 - Controls its motion in response

- Impedance-Control Algorithm $M\ddot{x} + B\dot{x} + Kx = f_{\text{ext}}$ $\tau = J^{\text{T}}(\theta) \left(\underbrace{\tilde{\Lambda}(\theta)\ddot{x} + \tilde{\eta}(\theta, \dot{x})}_{\text{arm dynamics compensation}} - \underbrace{(M\ddot{x} + B\dot{x} + Kx)}_{f_{\text{ext}}} \right)$
- Admittance-Control Algorithm

$$\ddot{x}_d = M^{-1}(f_{\text{ext}} - B\dot{x} - Kx)$$

$$\dot{x} = J(\theta)\dot{\theta}$$

 $\ddot{\theta}_d = J^{\dagger}(\theta)(\ddot{x}_d - \dot{J}(\theta)\dot{\theta})$

Use inverse dynamics to calculate the commanded joint forces and torques

Summary

- Task-space motion control
- Force control
- Impedance control

Further Reading

• Chapter 11 in Kevin M. Lynch and Frank C. Park. Modern Robotics: Mechanics, Planning, and Control. 1st Edition, 2017.