

CS 6301 Special Topics: Introduction to Robot Manipulation and Navigation

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Wheeled Mobile Robots



https://stanleyinnovation.com/productsservices/robotics/robotic-mobility-platforms/



https://www.mdpi.com/1424-8220/21/22/7642



https://ozrobotics.com/shop/3wd-100mm-omni-wheel-mobile-arduino-robot-kit-10013/

Wheeled Mobile Robots

- Kinematic model of a wheeled mobile robot
 - A chassis-fixed frame (b) relative to a fixed space frame (s) $T_{sb} \in SE(2)$
 - Represent T_{sb} by three coordinates $q=(\phi,x,y)$
 - Velocity of the chassis $\,\dot{q}=(\phi,\dot{x},\dot{y})\,$
 - Chassis' planar twist $\mathcal{V}_b = (\omega_{bz}, v_{bx}, v_{by})$

$$T^{-1}\dot{T} = \begin{bmatrix} R^{\mathrm{T}} & -R^{\mathrm{T}}p \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{R} & \dot{p} \\ 0 & 0 \end{bmatrix}$$

$$= \begin{bmatrix} R^{\mathrm{T}}\dot{R} & R^{\mathrm{T}}\dot{p} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{R} & \dot{p} \\ 0 & 0 \end{bmatrix}$$

$$= \begin{bmatrix} R^{\mathrm{T}}\dot{R} & R^{\mathrm{T}}\dot{p} \\ 0 & 0 \end{bmatrix} \cdot$$

$$= \begin{bmatrix} [\omega_b] & v_b \\ 0 & 0 \end{bmatrix} \cdot$$

$$R^{\mathrm{T}}\dot{p} = v_b$$

$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\phi & \sin\phi \\ 0 & -\sin\phi & \cos\phi \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix}$$

Types of Wheeled Mobile Robots

Omindirectional

- No equality constraints on the chassis velocity $~\dot{q}=(\dot{\phi},\dot{x},\dot{y})$
- Omniwheels





- Pfaffian constraints $A(q)\dot{q}=0$
- Car-like robots
- Conventional wheels



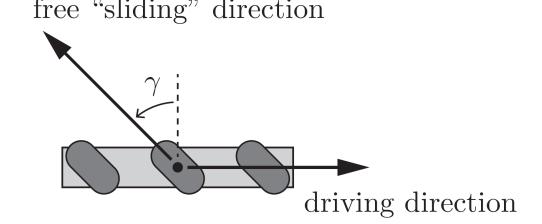




Linear velocity of the center of the wheel in a frame at the wheel

$$\begin{bmatrix} v_x \\ v_y \end{bmatrix} = v_{\text{drive}} \begin{bmatrix} 1 \\ 0 \end{bmatrix} + v_{\text{slide}} \begin{bmatrix} -\sin \gamma \\ \cos \gamma \end{bmatrix}$$
 free "sliding" direction
$$v_{\text{drive}} = v_x + v_y \tan \gamma,$$

$$v_{\text{slide}} = v_y / \cos \gamma.$$



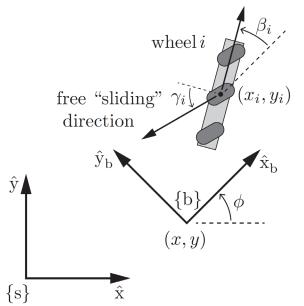
Driving angular speed
$$u=rac{v_{
m drive}}{r}=rac{1}{r}(v_x+v_y an\gamma)$$
 $extstyle = extstyle T U$

$$u_i = h_i(\phi)\dot{q} =$$

wheel frame Cross product

$$\left[\frac{1}{r_i} \frac{\tan \gamma_i}{r_i} \right] \left[\begin{array}{ccc} \cos \beta_i & \sin \beta_i \\ -\sin \beta_i & \cos \beta_i \end{array} \right] \left[\begin{array}{ccc} -y_i & 1 & 0 \\ x_i & 0 & 1 \end{array} \right] \left[\begin{array}{ccc} 1 & 0 & 0 \\ 0 & \cos \phi & \sin \phi \\ 0 & -\sin \phi & \cos \phi \end{array} \right] \left[\begin{array}{c} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{array} \right]$$

driving direction



$$\mathcal{V}_b = \begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\phi & \sin\phi \\ 0 & -\sin\phi & \cos\phi \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix}$$

$$h_i(\phi) = \frac{1}{r_i \cos \gamma_i} \begin{bmatrix} x_i \sin(\beta_i + \gamma_i) - y_i \cos(\beta_i + \gamma_i) \\ \cos(\beta_i + \gamma_i + \phi) \\ \sin(\beta_i + \gamma_i + \phi) \end{bmatrix}^{\mathrm{T}}$$

For m omnidirectional wheels

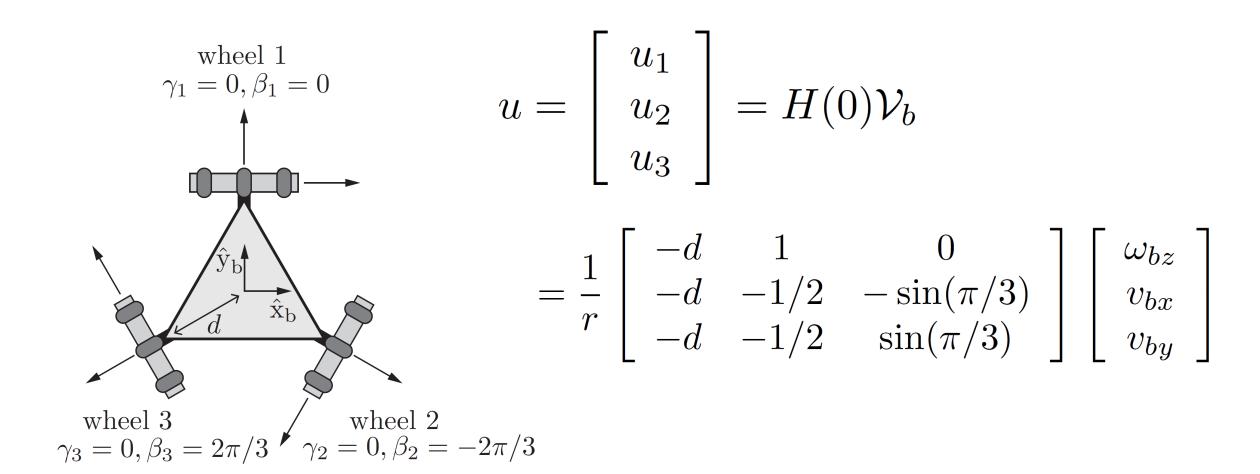
Driving angular speed

$$u = H(\phi)\dot{q} = \begin{bmatrix} h_1(\phi) \\ h_2(\phi) \\ \vdots \\ h_m(\phi) \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} \qquad H(\phi) \in \mathbb{R}^{m \times 3}$$

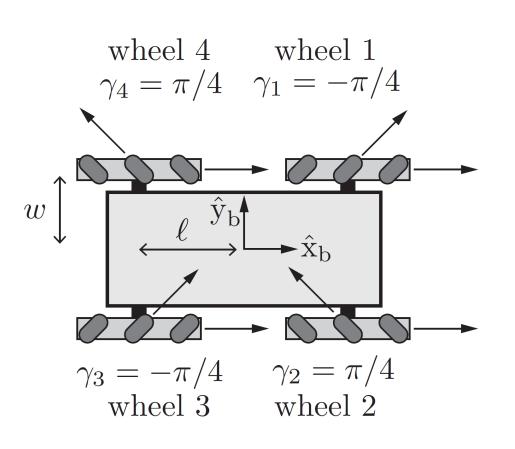
$$H(\phi) \in \mathbb{R}^{m \times 3}$$

$$u = H(0)\mathcal{V}_b = \begin{bmatrix} h_1(0) \\ h_2(0) \\ \vdots \\ h_m(0) \end{bmatrix} \begin{bmatrix} \\ \\ \end{bmatrix}$$

$$u = H(0)\mathcal{V}_b = \begin{bmatrix} h_1(0) \\ h_2(0) \\ \vdots \\ h_m(0) \end{bmatrix} \begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix} \quad \mathcal{V}_b = \begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\phi & \sin\phi \\ 0 & -\sin\phi & \cos\phi \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix}$$



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$$u = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} = H(0)\mathcal{V}_b$$

$$= \frac{1}{r} \begin{bmatrix} -\ell - w & 1 & -1 \\ \ell + w & 1 & 1 \\ \ell + w & 1 & -1 \\ -\ell - w & 1 & 1 \end{bmatrix} \begin{bmatrix} \omega_{bz} \\ v_{bx} \\ v_{by} \end{bmatrix}$$

The unicycle

• Configuration of the wheel $\ q = (\phi, x, y, \theta)$

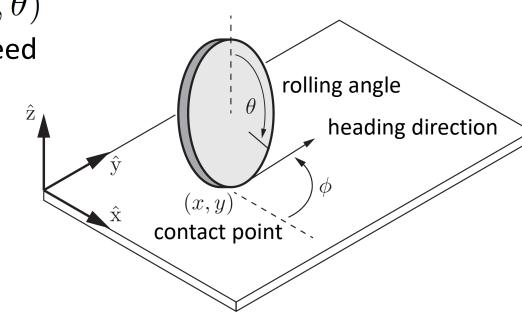
 Control input: forward-backward driving speed u1 and heading direction turning speed u2

Kinematic equations of motion

$$\dot{q} = \left[egin{array}{c} \dot{\phi} \ \dot{x} \ \dot{y} \ \dot{ heta} \end{array}
ight] = \left[egin{array}{ccc} 0 & 1 \ r\cos\phi & 0 \ r\sin\phi & 0 \ 1 & 0 \end{array}
ight] \left[egin{array}{c} u_1 \ u_2 \end{array}
ight]$$

$$= G(q)u = g_1(q)u_1 + g_2(q)u_2$$

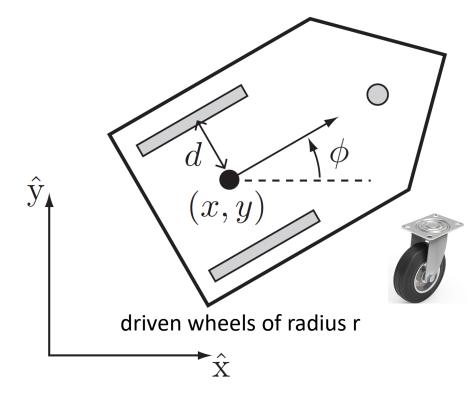
g1, g2 are called tangent vector fields (control vector fields, velocity vector fields)



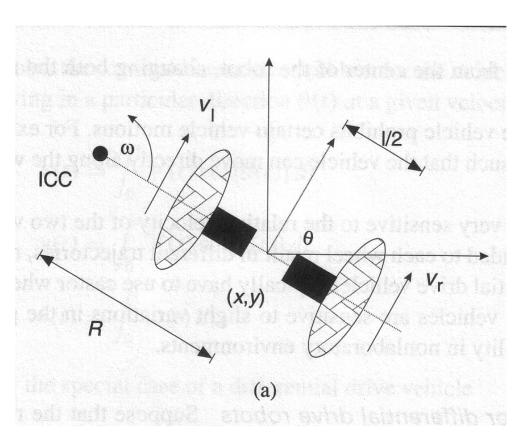
$$-u_{1,\max} \le u_1 \le u_{1,\max}$$

$$-u_{2,\max} \le u_2 \le u_{2,\max}$$

- The Differential-Drive Robot (diff-drive)
 - Two independently driven wheels of radius r that rotate about the same axis
 - One or more caster wheels, ball casters or lowfriction slides that keep the car horizontal



The Differential-Drive Robot



$$\omega (R + l/2) = V_r$$

$$\omega (R - l/2) = V_l$$

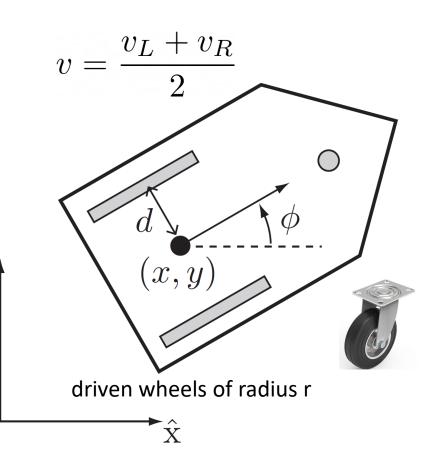
$$R = \frac{l}{2} \frac{V_l + V_r}{V_r - V_l}; \quad \omega = \frac{V_r - V_l}{l};$$

https://www.cs.columbia.edu/~allen/F17/NOTES/icckinematics.pdf

Kinematic equations

$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \\ \dot{\theta}_{\rm L} \\ \dot{\theta}_{\rm R} \end{bmatrix} = \begin{bmatrix} -r/2d & r/2d \\ \frac{r}{2}\cos\phi & \frac{r}{2}\cos\phi \\ \frac{r}{2}\sin\phi & \frac{r}{2}\sin\phi \\ 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_{\rm L} \\ u_{\rm R} \end{bmatrix}$$

angular speed of the left wheel and the right wheel



Diff-drive

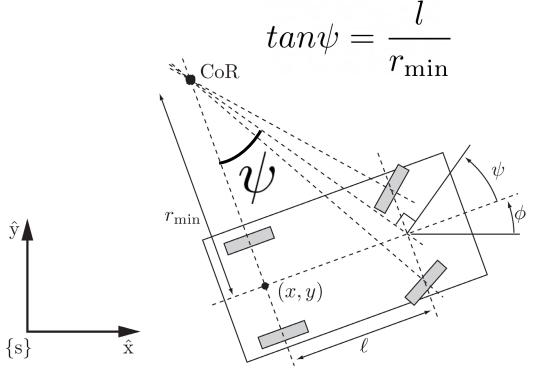
$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -r/2d & r/2d \\ \frac{r}{2}\cos\phi & \frac{r}{2}\cos\phi \\ \frac{r}{2}\sin\phi & \frac{r}{2}\sin\phi \end{bmatrix} \begin{bmatrix} u_{\rm L} \\ u_{\rm R} \end{bmatrix} \hat{y}$$

The car-like robot

- Configuration $q=(\phi,x,y,\psi)$ Heading direction ϕ
- ullet Steering angle ψ
- Control inputs: forward speed v and angular speed w of the steering angle

Kinematics

$$\dot{q} = \left[egin{array}{c} \dot{\phi} \ \dot{x} \ \dot{y} \ \dot{\psi} \end{array}
ight] = \left[egin{array}{c} (an\psi)/\ell & 0 \ \cos\phi & 0 \ \sin\phi & 0 \ 0 & 1 \end{array}
ight] \left[egin{array}{c} v \ w \end{array}
ight]$$



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- The car-like robot
 - Simplify the control to steering angle $\,\psi\,$
 - Control inputs (v, ω) can be converted to (v, ψ)

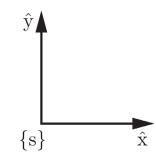
Forward speed

Rate of rotation

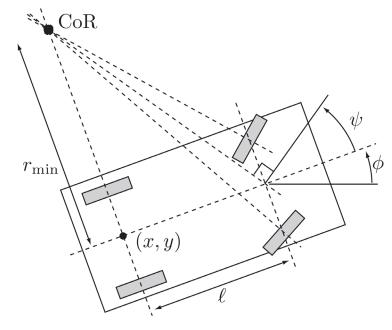
$$\psi = \tan^{-1} \left(\frac{\ell \omega}{v} \right)$$

Simplified car kinematics

$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} = G(q)u = \begin{bmatrix} 0 & 1 \\ \cos \phi & 0 \\ \sin \phi & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$



$$v = r_{\min}\omega$$



Car kinematics

$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} = G(q)u = \begin{bmatrix} 0 & 1 \\ \cos \phi & 0 \\ \sin \phi & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$

Nonholonomic constraint

$$\dot{x} = v\cos\phi,$$

$$\dot{y} = v\sin\phi,$$

$$A(q)\dot{q} = [0 \sin \phi - \cos \phi]\dot{q} = \dot{x}\sin \phi - \dot{y}\cos \phi = 0.$$

Canonical simplified model

• Unicycle
$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ r\cos\phi & 0 \\ r\sin\phi & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} \qquad u_1 = \frac{v}{r}, \qquad u_2 = \omega$$

$$u_1 = \frac{v}{r}, \qquad u_2 = \omega$$

$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} = G(q)u = \begin{bmatrix} 0 & 1 \\ \cos \phi & 0 \\ \sin \phi & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$

- Canonical simplified model
 - Diff-drive

$$\dot{q} = \left[egin{array}{c} \dot{\phi} \\ \dot{x} \\ \dot{y} \\ \dot{ heta}_{
m L} \\ \dot{ heta}_{
m R} \end{array}
ight] = \left[egin{array}{c} -r/2d & r/2d \\ rac{r}{2}\cos\phi & rac{r}{2}\cos\phi \\ rac{r}{2}\sin\phi & rac{r}{2}\sin\phi \\ 1 & 0 \\ 0 & 1 \end{array}
ight] \left[egin{array}{c} u_{
m L} \\ u_{
m R} \end{array}
ight]$$

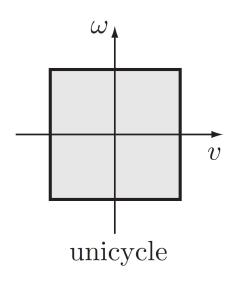
$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} = G(q)u = \begin{bmatrix} 0 & 1 \\ \cos \phi & 0 \\ \sin \phi & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$

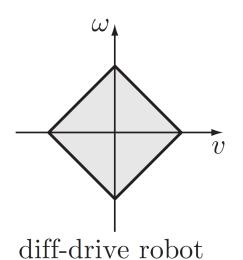
$$u_{\rm L} = \frac{v - \omega d}{r}$$
$$u_{\rm R} = \frac{v + \omega d}{r}$$

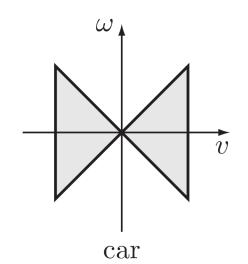
$$u_{\rm R} = \frac{v + \omega d}{r}$$

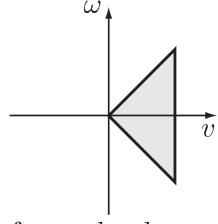
Canonical simplified model

$$\dot{q} = \begin{bmatrix} \dot{\phi} \\ \dot{x} \\ \dot{y} \end{bmatrix} = G(q)u = \begin{bmatrix} 0 & 1 \\ \cos \phi & 0 \\ \sin \phi & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$









forward-only car

- The process of estimating the chassis configuration q from the wheel motions
 - Wheel rotation sensing is available on all mobile robots
 - Estimation errors tend to accumulate over time
 - Supplement odometry with other position sensors such as GPS, laser, etc.

• Estimate the new chassis configuration q_{k+1} given the previous configuration q_k and the change in wheel angles $\Delta \theta$

• Let $\Delta \theta_i$ be the change in wheel i's driving angle

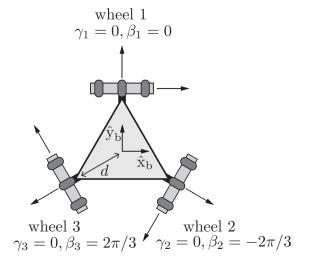
$$\dot{\theta}_i = \Delta \theta_i / \Delta t$$
 set $\Delta t = 1$ $\dot{\theta}_i = \Delta \theta_i$

For omnidirectional mobile robots

$$\Delta \theta = H(0) \mathcal{V}_b$$
$$\mathcal{V}_b = H^{\dagger}(0) \Delta \theta = F \Delta \theta$$

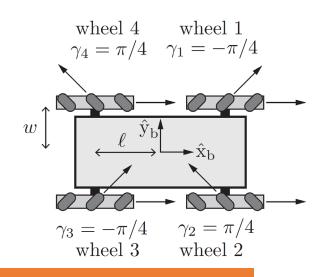
For three-omniwheel robot

$$\mathcal{V}_b = F\Delta\theta = r \begin{bmatrix} -1/(3d) & -1/(3d) & -1/(3d) \\ 2/3 & -1/3 & -1/3 \\ 0 & -1/(2\sin(\pi/3)) & 1/(2\sin(\pi/3)) \end{bmatrix} \Delta\theta$$



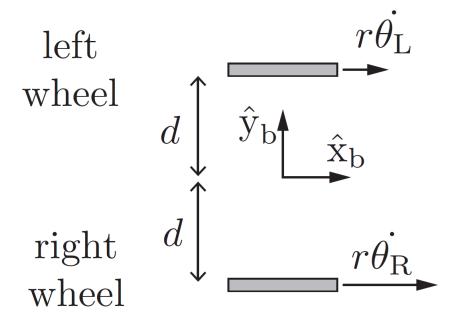
For four-mecanum-wheel robot

$$\mathcal{V}_{b} = F\Delta\theta = \frac{r}{4} \begin{bmatrix} -1/(\ell+w) & 1/(\ell+w) & 1/(\ell+w) & -1/(\ell+w) \\ 1 & 1 & 1 & 1 \\ -1 & 1 & -1 & 1 \end{bmatrix} \Delta\theta \quad \text{w.s.} \hat{\mathbf{y}}_{b}$$



• Diff-drive robot

$$\mathcal{V}_b = F\Delta\theta = r \begin{bmatrix} -1/(2d) & 1/(2d) \\ 1/2 & 1/2 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \Delta\theta_{\rm L} \\ \Delta\theta_{\rm R} \end{bmatrix}$$



$$\mathcal{V}_b = F\Delta\theta$$

$$\mathcal{V}_{b6} = (0, 0, \omega_{bz}, v_{bx}, v_{by}, 0)$$

if
$$\omega_{bz} = 0$$
, $\Delta q_b = \begin{bmatrix} \Delta \phi_b \\ \Delta x_b \\ \Delta y_b \end{bmatrix} = \begin{bmatrix} 0 \\ v_{bx} \\ v_{by} \end{bmatrix}$

$$T_{bb'} = e^{[\mathcal{V}_{b6}]}$$

$$e^{[S]\theta} = \begin{bmatrix} e^{[\omega]\theta} & G(\theta)v \\ 0 & 1 \end{bmatrix}$$

if
$$\omega_{bz} \neq 0$$
, $\Delta q_b = \begin{bmatrix} \Delta \phi_b \\ \Delta x_b \\ \Delta y_b \end{bmatrix} = \begin{bmatrix} \omega_{bz} \\ (v_{bx} \sin \omega_{bz} + v_{by} (\cos \omega_{bz} - 1))/\omega_{bz} \\ (v_{by} \sin \omega_{bz} + v_{bx} (1 - \cos \omega_{bz}))/\omega_{bz} \end{bmatrix}$

• In fixed frame {s}

$$\Delta q = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \phi_k & -\sin \phi_k \\ 0 & \sin \phi_k & \cos \phi_k \end{bmatrix} \Delta q_b$$

Updated odometry

$$q_{k+1} = q_k + \Delta q$$

Summary

Omnidirectional Wheeled Mobile Robots

Nonholonomic Wheeled Mobile Robots

Odometry

Further Reading

 Chapter 13 in Kevin M. Lynch and Frank C. Park. Modern Robotics: Mechanics, Planning, and Control. 1st Edition, 2017.

• G. Oriolo. Wheeled robots. In J. Baillieul and T. Samad, editors, Encyclopedia of Systems and Control. Springer-Verlag, 2015.

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