# Dynamics of Open Chains: A Single Rigid Body

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## **Robot Dynamics**

- Study motion of robots with the forces and torques that case them
- Equations of motion
  - A set of second-order differential equations

$$au = M( heta) \ddot{ heta} + h( heta, \dot{ heta})$$
 Joint variables  $heta \in \mathbb{R}^n$ 

Joint forces and torques  $\ au\in \mathbb{R}^n$   $M( heta)\in \mathbb{R}^{n imes n}$  a symmetric positive-definite mass matrix

 $h(\theta, \dot{\theta}) \in \mathbb{R}^n$ 

forces that lump together centripetal, Coriolis, gravity, and friction terms that depend on  $\theta$  and  $\dot{\theta}$ 

# Forward and Inverse Dynamics

- Forward dynamics
  - Given robot state ( heta, heta) and the joint forces and torques
  - Determine the robot's acceleration

$$\ddot{\theta} = M^{-1}(\theta) \left(\tau - h(\theta, \dot{\theta})\right)$$

- Inverse dynamics
  - Given robot state ( heta, heta) and a desired acceleration
  - Find the joint forces and torques

$$\tau = M(\theta)\ddot{\theta} + h(\theta, \dot{\theta})$$

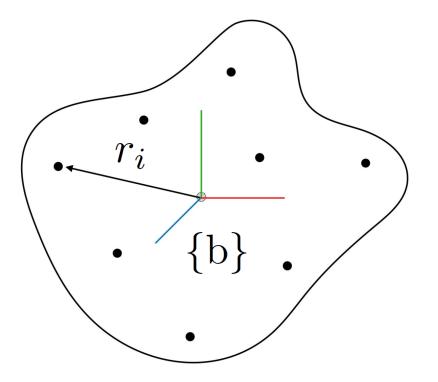
# Robot Dynamics

- Lagrangian formulation
  - Kinetic energy and potential energy
- Newton-Euler formulation
  - F = ma

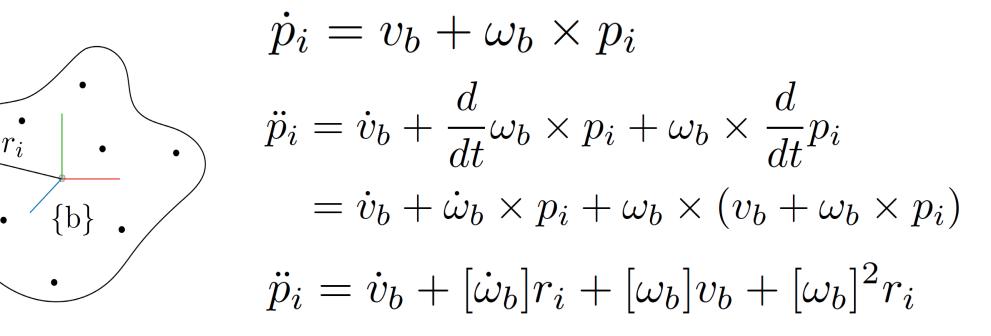
- A rigid body with a set of point masses
- Total mass  $\mathfrak{m} = \sum_i \mathfrak{m}_i$
- The origin of the body frame

Center of mass 
$$\sum_{i} \mathfrak{m}_{i} r_{i} = 0$$

• If some other point is chosen as origin, move the origin to  $(1/\mathfrak{m})\sum_i\mathfrak{m}_i r_i$ 



- Assume the body is moving with a body twist  $|\mathcal{V}_b| = (\omega_b, v_b)$
- $p_i(t)$  be the time-varying position of  $\mathfrak{m}_i$  , initially at  $r_i$  .



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• For a point mass  $f_i = \mathfrak{m}_i \ddot{p}_i$ 

$$f_i = \mathfrak{m}_i (\dot{v}_b + [\dot{\omega}_b]r_i + [\omega_b]v_b + [\omega_b]^2 r_i)$$

- Moment of the point mass  $m_i = [r_i]f_i$
- Total force and moment on the body

Wrench 
$$\mathcal{F}_b = \begin{bmatrix} m_b \\ f_b \end{bmatrix} = \begin{bmatrix} \sum_i m_i \\ \sum_i f_i \end{bmatrix}$$

• Linear dynamics

$$\begin{split} f_b &= \sum_i \mathfrak{m}_i (\dot{v}_b + [\dot{\omega}_b] r_i + [\omega_b] v_b + [\omega_b]^2 r_i) \\ &= \sum_i \mathfrak{m}_i (\dot{v}_b + [\omega_b] v_b) - \underbrace{\sum_i \mathfrak{m}_i [r_i] \dot{\omega}_b}_i + \underbrace{\sum_i \mathfrak{m}_i [r_i] [\omega_b] \omega_b}_i 0 \\ &= \sum_i \mathfrak{m}_i (\dot{v}_b + [\omega_b] v_b) \\ &= \mathfrak{m} (\dot{v}_b + [\omega_b] v_b). \end{split}$$

$$\sum_{i} \mathfrak{m}_{i}[r_{i}] = 0$$
$$[a] = -[a]^{\mathrm{T}}$$
$$[a]b = -[b]a$$
$$[a][b] = ([b][a])^{\mathrm{T}}$$

• Rotational dynamics

$$\begin{split} m_b &= \sum_{i} \mathfrak{m}_i [r_i] (\dot{v}_b + [\dot{\omega}_b] r_i + [\omega_b] v_b + [\omega_b]^2 r_i) \\ &= \underbrace{\sum_{i} \mathfrak{m}_i [r_i] \dot{v}_b}_{i} + \underbrace{\sum_{i} \mathfrak{m}_i [r_i] [\omega_b] v_b}_{i} \overset{0}{} \\ &+ \sum_{i} \mathfrak{m}_i [r_i] ([\dot{\omega}_b] r_i + [\omega_b]^2 r_i) \\ &= \sum_{i} \mathfrak{m}_i \left( -[r_i]^2 \dot{\omega}_b - [r_i]^T [\omega_b]^T [r_i] \omega_b \right) \\ &= \sum_{i} \mathfrak{m}_i \left( -[r_i]^2 \dot{\omega}_b - [\omega_b] [r_i]^2 \omega_b \right) \\ &= \left( -\sum_{i} \mathfrak{m}_i [r_i]^2 \right) \dot{\omega}_b + [\omega_b] \left( -\sum_{i} \mathfrak{m}_i [r_i]^2 \right) \omega_b \\ &= \mathcal{I}_b \dot{\omega}_b + [\omega_b] \mathcal{I}_b \omega_b, \end{split}$$

Body's rotational inertia matrix

$$\mathcal{I}_b = -\sum_i \mathfrak{m}_i [r_i]^2 \in \mathbb{R}^{3 \times 3}$$

Euler's equation for a rotating rigid body

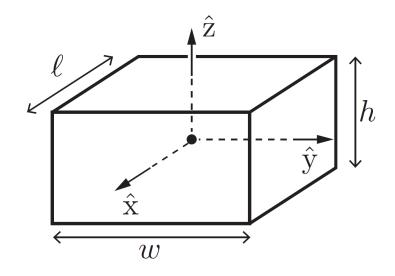
• Rotational inertia matrix  $\mathcal{I}_b = -\sum_i \mathfrak{m}_i [r_i]^2 \in \mathbb{R}^{3 \times 3}$ 

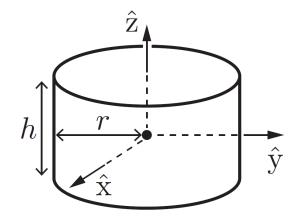
$$\begin{split} \mathcal{I}_{b} &= \begin{bmatrix} \sum \mathfrak{m}_{i}(y_{i}^{2}+z_{i}^{2}) & -\sum \mathfrak{m}_{i}x_{i}y_{i} & -\sum \mathfrak{m}_{i}x_{i}z_{i} \\ -\sum \mathfrak{m}_{i}x_{i}y_{i} & \sum \mathfrak{m}_{i}(x_{i}^{2}+z_{i}^{2}) & -\sum \mathfrak{m}_{i}y_{i}z_{i} \\ -\sum \mathfrak{m}_{i}x_{i}z_{i} & -\sum \mathfrak{m}_{i}y_{i}z_{i} & \sum \mathfrak{m}_{i}(x_{i}^{2}+y_{i}^{2}) \end{bmatrix} \\ &= \begin{bmatrix} \mathcal{I}_{xx} & \mathcal{I}_{xy} & \mathcal{I}_{xz} \\ \mathcal{I}_{xy} & \mathcal{I}_{yy} & \mathcal{I}_{yz} \\ \mathcal{I}_{xz} & \mathcal{I}_{yz} & \mathcal{I}_{zz} \end{bmatrix} . \\ \mathcal{I}_{xx} &= \int_{\mathcal{B}} (y^{2}+z^{2})\rho(x,y,z) \, dV & \mathcal{I}_{xy} &= -\int_{\mathcal{B}} xy\rho(x,y,z) \, dV \\ \mathcal{I}_{yy} &= \int_{\mathcal{B}} (x^{2}+z^{2})\rho(x,y,z) \, dV & \mathcal{I}_{xz} &= -\int_{\mathcal{B}} xz\rho(x,y,z) \, dV \\ \mathcal{I}_{zz} &= \int_{\mathcal{B}} (x^{2}+y^{2})\rho(x,y,z) \, dV & \mathcal{I}_{yz} &= -\int_{\mathcal{B}} yz\rho(x,y,z) \, dV \\ \mathbf{mass density function} & \rho(x, y, z) \end{split}$$

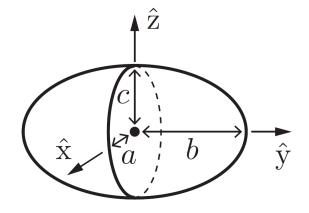
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- Principal axes of inertia: eigenvectors and eigenvalues of  $\mathcal{I}_b$ 
  - Directions given by eigenvectors
  - Eigenvalues are principal moments of inertia
- If the principal axes are aligned with the axes of {b},  $\mathcal{I}_b$  is a diagonal matrix

rotational dynamics 
$$m_b = \begin{bmatrix} \mathcal{I}_{xx}\dot{\omega}_x + (\mathcal{I}_{zz} - \mathcal{I}_{yy})\omega_y\omega_z \\ \mathcal{I}_{yy}\dot{\omega}_y + (\mathcal{I}_{xx} - \mathcal{I}_{zz})\omega_x\omega_z \\ \mathcal{I}_{zz}\dot{\omega}_z + (\mathcal{I}_{yy} - \mathcal{I}_{xx})\omega_x\omega_y \end{bmatrix} \quad \omega_b = (\omega_x, \omega_y, \omega_z)$$







rectangular parallelepiped: volume = abc,  $\mathcal{I}_{xx} = \mathfrak{m}(w^2 + h^2)/12$ ,  $\mathcal{I}_{yy} = \mathfrak{m}(\ell^2 + h^2)/12$ ,  $\mathcal{I}_{zz} = \mathfrak{m}(\ell^2 + w^2)/12$  circular cylinder: volume =  $\pi r^2 h$ ,  $\mathcal{I}_{xx} = \mathfrak{m}(3r^2 + h^2)/12$ ,  $\mathcal{I}_{yy} = \mathfrak{m}(3r^2 + h^2)/12$ ,  $\mathcal{I}_{zz} = \mathfrak{m}r^2/2$  ellipsoid: volume =  $4\pi abc/3$ ,  $\mathcal{I}_{xx} = \mathfrak{m}(b^2 + c^2)/5$ ,  $\mathcal{I}_{yy} = \mathfrak{m}(a^2 + c^2)/5$ ,  $\mathcal{I}_{zz} = \mathfrak{m}(a^2 + b^2)/5$ 

- Inertia matrix in a rotated frame {c}
- Kinetic energy is the same in different frame

$$\frac{1}{2}\omega_c^{\mathrm{T}}\mathcal{I}_c\omega_c = \frac{1}{2}\omega_b^{\mathrm{T}}\mathcal{I}_b\omega_b$$

$$= \frac{1}{2}(R_{bc}\omega_c)^{\mathrm{T}}\mathcal{I}_b(R_{bc}\omega_c)$$

$$= \frac{1}{2}\omega_c^{\mathrm{T}}(R_{bc}^{\mathrm{T}}\mathcal{I}_bR_{bc})\omega_c.$$

$$\mathcal{I}_c = R_{bc}^{\mathrm{T}} \mathcal{I}_b R_{bc}$$

### Steiner's theorem

• The inertia matrix  $\mathcal{I}_q$  about a frame aligned with {b}, but at a point in {b}  $q = (q_x, q_y, q_z)$ , is related to the inertia matrix calculated at the center of mass by

$$\mathcal{I}_q = \mathcal{I}_b + \mathfrak{m}(q^{\mathrm{T}}qI - qq^{\mathrm{T}})$$

• Parallel-axis theorem: the scalar inertia  $\mathcal{I}_d$  about an axis parallel to, but a distance d from, an axis through the center of mass is

$$\mathcal{I}_d = \mathcal{I}_{\rm cm} + \mathfrak{m} d^2$$

• Change of reference frame

$$\mathcal{I}_c = R_{bc}^{\mathrm{T}} \mathcal{I}_b R_{bc}$$

$$\mathcal{I}_q = \mathcal{I}_b + \mathfrak{m}(q^{\mathrm{T}}qI - qq^{\mathrm{T}})$$

- Linear dynamics  $f_b = \mathfrak{m}(\dot{v}_b + [\omega_b]v_b)$
- Rotation dynamics  $m_b = \mathcal{I}_b \dot{\omega}_b + [\omega_b] \mathcal{I}_b \omega_b$

$$\begin{bmatrix} m_b \\ f_b \end{bmatrix} = \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix} \begin{bmatrix} \dot{\omega}_b \\ \dot{v}_b \end{bmatrix} + \begin{bmatrix} [\omega_b] & 0 \\ 0 & [\omega_b] \end{bmatrix} \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix} \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$$
$$\begin{bmatrix} v]v = v \times v = 0 \text{ and } [v]^{\mathrm{T}} = -[v]$$
$$\begin{bmatrix} m_b \\ f_b \end{bmatrix} = \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix} \begin{bmatrix} \dot{\omega}_b \\ \dot{v}_b \end{bmatrix} + \begin{bmatrix} [\omega_b] & [v_b] \\ 0 & [\omega_b] \end{bmatrix} \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix} \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$$
$$= \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix} \begin{bmatrix} \dot{\omega}_b \\ \dot{v}_b \end{bmatrix} - \begin{bmatrix} [\omega_b] & 0 \\ [v_b] & [\omega_b] \end{bmatrix}^{\mathrm{T}} \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix} \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$$

Body twist 
$$\mathcal{V}_b = \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$$
 Body wrench  $\mathcal{F}_b = \begin{bmatrix} m_b \\ f_b \end{bmatrix}$   
spatial inertia matrix  $\mathcal{G}_b \in \mathbb{R}^{6 \times 6}$   $\mathcal{G}_b = \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix}$   
kinetic energy  $= \frac{1}{2}\omega_b^{\mathrm{T}}\mathcal{I}_b\omega_b + \frac{1}{2}\mathfrak{m}v_b^{\mathrm{T}}v_b = \frac{1}{2}\mathcal{V}_b^{\mathrm{T}}\mathcal{G}_b\mathcal{V}_b$   
spatial momentum  $\mathcal{P}_b \in \mathbb{R}^6$   $\mathcal{P}_b = \begin{bmatrix} \mathcal{I}_b\omega_b \\ \mathfrak{m}v_b \end{bmatrix} = \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathfrak{m}I \end{bmatrix} \begin{bmatrix} \omega_b \\ v_b \end{bmatrix} = \mathcal{G}_b\mathcal{V}_b$ 

• Lie bracket of two twists  $\mathcal{V}_1 = (\omega_1, v_1)$  and  $\mathcal{V}_2 = (\omega_2, v_2)$ 

$$\begin{bmatrix} [\omega_1] & 0 \\ [v_1] & [\omega_1] \end{bmatrix} \begin{bmatrix} \omega_2 \\ v_2 \end{bmatrix} = [\mathrm{ad}_{\mathcal{V}_1}]\mathcal{V}_2 = \mathrm{ad}_{\mathcal{V}_1}(\mathcal{V}_2) \in \mathbb{R}^6$$
$$[\mathrm{ad}_{\mathcal{V}}] = \begin{bmatrix} [\omega] & 0 \\ [v] & [\omega] \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$

• Dynamic equations for a single rigid body

$$\begin{aligned} \mathcal{F}_b &= \mathcal{G}_b \dot{\mathcal{V}}_b - \mathrm{ad}_{\mathcal{V}_b}^{\mathrm{T}}(\mathcal{P}_b) \\ &= \mathcal{G}_b \dot{\mathcal{V}}_b - [\mathrm{ad}_{\mathcal{V}_b}]^{\mathrm{T}} \mathcal{G}_b \mathcal{V}_b \end{aligned}$$

• Moment equation for a rigid body

$$m_b = \mathcal{I}_b \dot{\omega}_b - [\omega_b]^{\mathrm{T}} \mathcal{I}_b \omega_b$$

# Dynamics in Other Frames

• The kinetic energy is independent of frames

$$\frac{1}{2} \mathcal{V}_{a}^{\mathrm{T}} \mathcal{G}_{a} \mathcal{V}_{a} = \frac{1}{2} \mathcal{V}_{b}^{\mathrm{T}} \mathcal{G}_{b} \mathcal{V}_{b}$$
$$= \frac{1}{2} ([\mathrm{Ad}_{T_{ba}}] \mathcal{V}_{a})^{\mathrm{T}} \mathcal{G}_{b} [\mathrm{Ad}_{T_{ba}}] \mathcal{V}_{a}$$
$$= \frac{1}{2} \mathcal{V}_{a}^{\mathrm{T}} \underbrace{[\mathrm{Ad}_{T_{ba}}]^{\mathrm{T}} \mathcal{G}_{b} [\mathrm{Ad}_{T_{ba}}]}_{\mathcal{G}_{a}} \mathcal{V}_{a};$$

$$\operatorname{Ad}_{T}] = \left[ \begin{array}{cc} R & 0\\ [p]R & R \end{array} \right] \in \mathbb{R}^{6 \times 6}$$

- The spatial inertia matrix  $\mathcal{G}_a = [\mathrm{Ad}_{T_{ba}}]^{\mathrm{T}} \mathcal{G}_b[\mathrm{Ad}_{T_{ba}}]$
- Equations of motion in frame {a}

$$\mathcal{F}_a = \mathcal{G}_a \dot{\mathcal{V}}_a - [\mathrm{ad}_{\mathcal{V}_a}]^{\mathrm{T}} \mathcal{G}_a \mathcal{V}_a$$

# Summary

- Dynamics of a single rigid body
  - Linear dynamics
  - Rotational dynamics

$$\mathcal{F}_{b} = \mathcal{G}_{b} \dot{\mathcal{V}}_{b} - \operatorname{ad}_{\mathcal{V}_{b}}^{\mathrm{T}}(\mathcal{P}_{b})$$

$$= \mathcal{G}_{b} \dot{\mathcal{V}}_{b} - [\operatorname{ad}_{\mathcal{V}_{b}}]^{\mathrm{T}} \mathcal{G}_{b} \mathcal{V}_{b}$$

# Further Reading

• Chapter 8 in Kevin M. Lynch and Frank C. Park. Modern Robotics: Mechanics, Planning, and Control. 1st Edition, 2017.